

# Topology optimization for staged construction with applications to additive manufacturing

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## Context – AATiD consortium

Develop advanced technologies for design and 3-D printing of optimized complex aero-structures made of Titanium alloys, Ti-6Al-4V

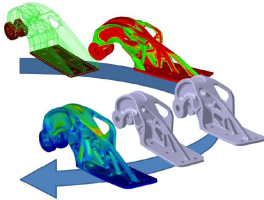
Detailed goals:

- Identify cost-effective parts, material qualification, optimize process, simulate process, welding of printed parts, ...
- Use **topology optimization** to achieve superior aero-structures design compared with traditional design, in terms of weight, cost and performance;
- **Embed printing technologies' limitations in the structural design process.**



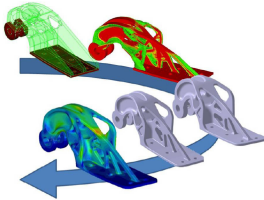
# Coupling TopOpt and Titanium AM

Airbus A320 nacelle hinge bracket [Tomlin and Meyer, 2011]:

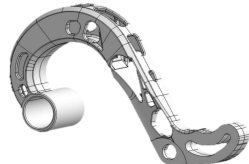
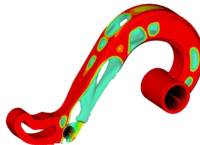


# Coupling TopOpt and Titanium AM

Airbus A320 nacelle hinge bracket [Tomlin and Meyer, 2011]:



IAI Gulfstream G250 gooseneck hinge [Muir, 2013]:



# Challenges in AM

Additive manufacturing typically requires **extensive support material** to prevent curling and distortion:

- Support overhang / inclination angle;
- Support horizontal bridging distances;
- Improve heat transfer.

Support material **counter-balances achievements of optimal design**:

- Longer build time, more material usage;
- Extensive rework required for removing supports;
- Difficulties in clearing supports in internal holes;
- Compromise on stiffness-to-weight.

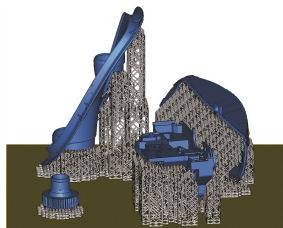
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Support structure (Materialise)

## Dealing with overhang limitations

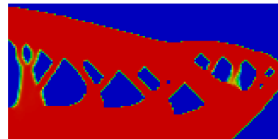
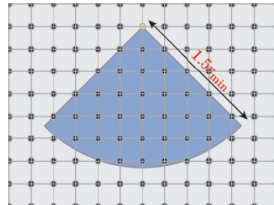
Necessary to embed the support requirement into the optimization

- Post-process an optimized design?
- Optimize for no-support?
- Optimize for minimum support?
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Use projection method to require support  
in specified angle [Gaynor, 2015] →



# Dealing with overhang limitations

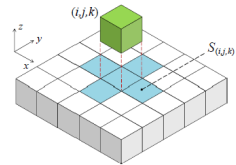
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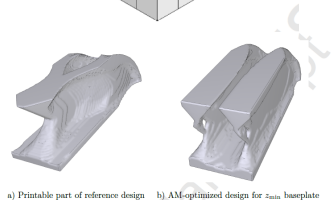
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Use AM-filter to ensure that material is supported [Langelaar, 2016] →



# Current research

**Goal:** Derive a procedure that can account for a given overhang limitation

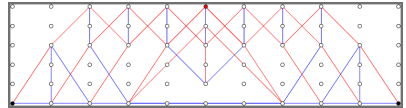
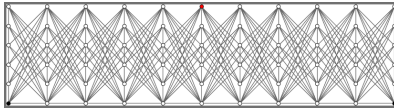
## Desired features:

- Can generate designs with no support;
- Can generate designs with limited support;
- To be investigated in 2-D but extendable to 3-D;
- Minimal compromise on performance  $\equiv$  stiffness-to-weight trade-off.

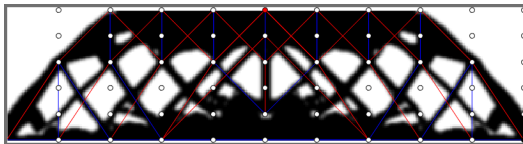
# Virtual skeleton approach – briefly

**Main idea:** allowable directions defined on a discrete line model (truss...) → virtual scaffold for continuum topology optimization

AM-oriented truss optimization



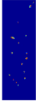
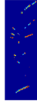

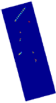
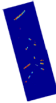


Topology optimization prioritized on virtual skeleton

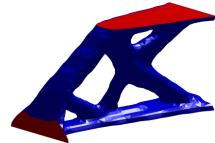


# Virtual skeleton approach – briefly

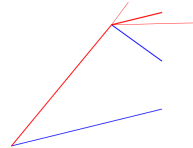
Table 4: Half MBB beam results

Case	Results	Layout	Gradient	Ref. gradient
Baseline	$c = 166.49$ UP = 6.09% for $90^\circ$ UP = 4.74% for $-75^\circ$		N/A	N/A
Print at $90^\circ$	$c = 169.63$ PD = 0.32% UP = 2.5%			
Print at $-75^\circ$	$c = 170.17$ PD = 2.21% UP = 2.26%			

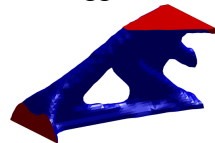
Standard



Truss



Suggested



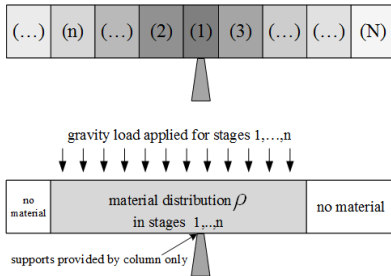
# Staged construction – balanced cantilever



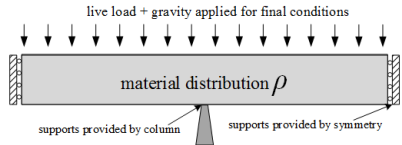
# Topology optimization for staged construction

Looking at the design of a balanced cantilever bridge:

## During construction



## Final conditions



# Topology optimization for staged construction

$$\min_{\rho} \quad f(\bar{\rho}) = \mathbf{f}_f^T \mathbf{u}_f + \sum_{n=1}^{N_{STG}} \theta_n \mathbf{f}_n^T \mathbf{u}_n$$

$$\text{s.t.:} \quad g(\bar{\rho}) = \sum_{e=1}^{N_E} \bar{\rho}_e v_e - V^* \leq 0$$

$$0 < \rho_{min} \leq \rho_e \leq 1, \quad e = 1, \dots, N_E$$

$$\text{with:} \quad \mathbf{K}_f \mathbf{u}_f = \mathbf{f}_f$$

$$\mathbf{K}_n \mathbf{u}_n = \mathbf{f}_n \quad n = 1, \dots, N_{STG}$$










Remarks:

- We have  $N_{STG}$  construction stages, with unique stiffness matrices, boundary conditions and loads
- We use **standard** topology optimization “ingredients”: SIMP, density filter, MMA, Heaviside projection (if necessary)



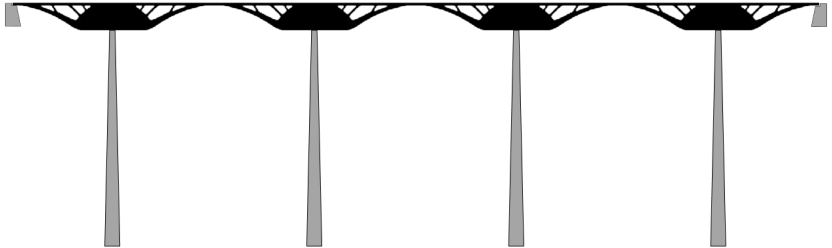
# Topology optimization for staged construction

Results of the staged construction approach, balanced cantilever bridge:

stages	optimized layout	comments
N/A		baseline design
		low $\theta$ , volume active
		high $\theta$ , volume inactive
		low $\theta$ , volume active
		high $\theta$ , volume inactive

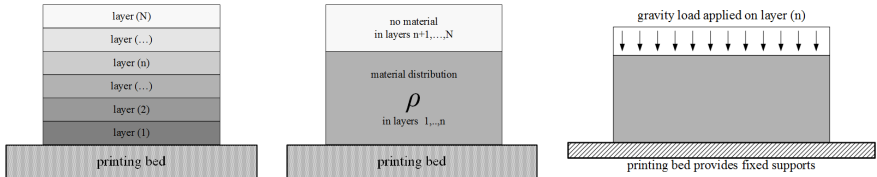
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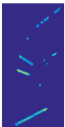

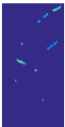

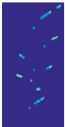


# Additive manufacturing as “staged construction”






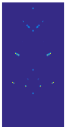
We see AM as a “layered” or “sliced” construction process:




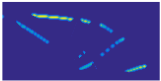



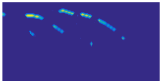
# Preliminary results – half MBB

slicing fractions	$\mathbf{f}_f^T \mathbf{u}_f$	$NSVF$	optimized layout	non-supported regions
N/A	72.8921	0.0061		
[80, 120] / 160	80.7397	0.0028		
[50, ..., 150@20] / 160	76.4435	0.0044		

## Preliminary results – cantilever

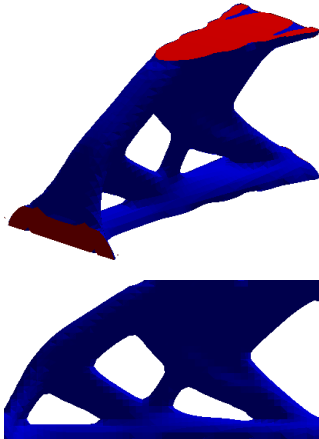
slicing fractions	$\mathbf{f}_f^T \mathbf{u}_f$	$NSVF$	optimized layout	non-supported regions
N/A	56.4807	0.0046		
[80, 100, 120] / 160	60.8694	0.0021		
[80, 90, 100, 110] / 160	59.4172	0.0018		

## Preliminary results – half MBB

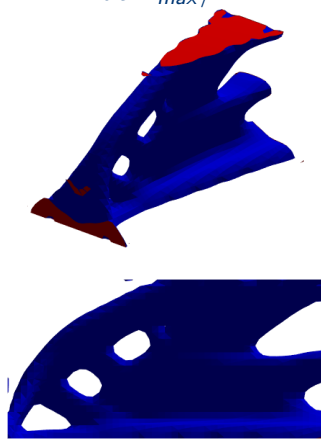
slicing fractions	$\mathbf{f}_f^T \mathbf{u}_f$	$NSVF$	optimized layout	non-supported regions
N/A	72.8921	0.0112		
70/80	85.0811	0.0027		
[70, 80] /80	81.0217	0.0061		

# Preliminary results – 3-D cantilever

Standard



Sliced approach  
at  $Z_{max}/2$



## Conclusions and outlook

- Simple approach, uses standard top-opt procedures
- Possibility for control: slicing pattern, penalties  $\theta_n$
- Straightforward implementation in pixel/voxel based top-opt, can extend to account for actual manufacturing process
- Buildability not 100% guaranteed, some post-processing may be required
- Compromise on optimized performance
- Cost of multiple simulations per design cycle
- No need for black-and-white convergence??? revival of gray material???



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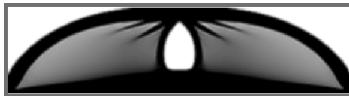
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**Thank you for listening**

# References I



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